

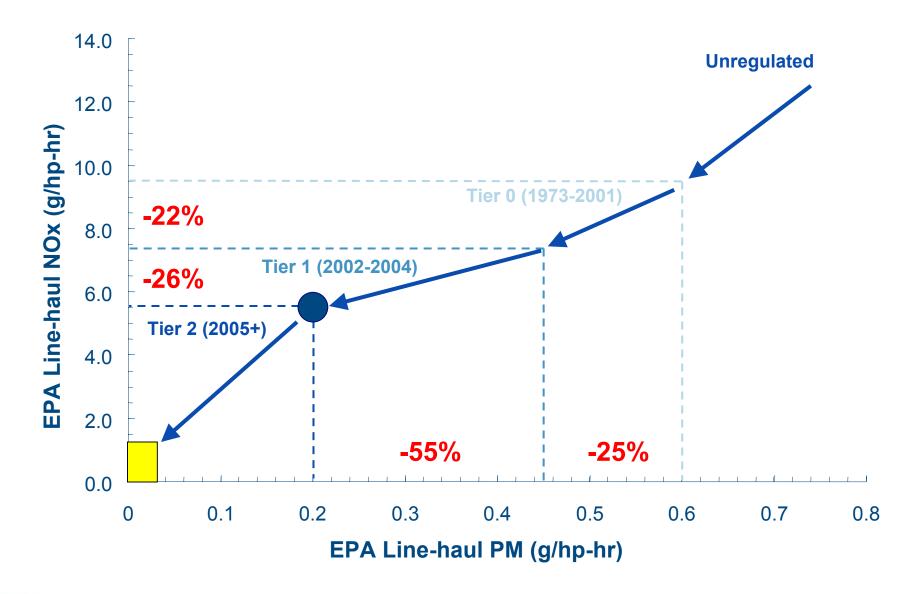
- → Where we are & where are we going
- → Tier 4 PM
- → Tier 4 NOx
- → Space & other constraints
- → Operational impact
- → Development requirements
- **→** Summary



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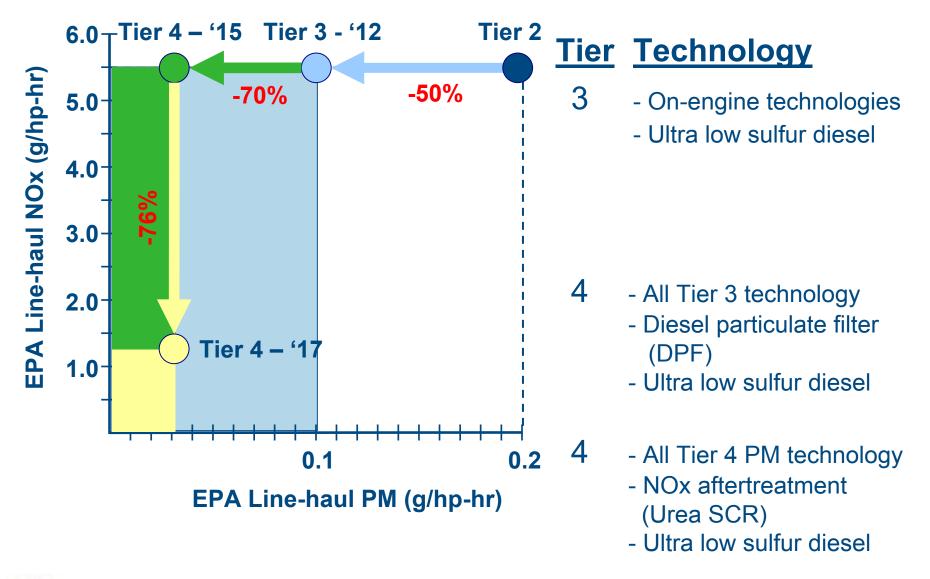


Where we have come from





Where we are going



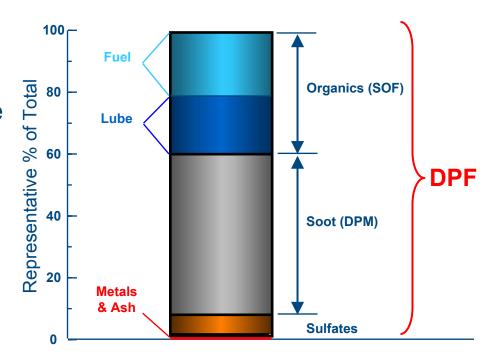


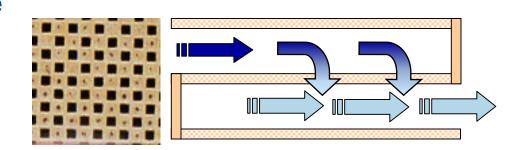
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Diesel Particulate Filter

- Captures all forms of particulate matter
- 90+% PM reductions are achievable
- Captured material must be periodically burned off (regenerated)
 - Avoid high back pressure
 - SFC penalty
- Technology path defined
- Significant engineering challenge
- Logistics/handling challenges:
 - Size/weight/handling equipment
 - May require crane for change out







PM Aftertreatment Concerns

Consumables:

- 1 to 2 % SFC increase . . . 35 70 tons/year of CO₂
 - added backpressure
 - regeneration energy

Maintenance:

- Ash cleaning every 180 days a must to match service intervals
 - Similar to power cylinder replacement (will require crane)
 - UX exchange process
 - Waste handling & disposal

Durability:

Anticipate replacement of DPF at end of useful life (engine overhaul)

Logistics:

- DPF maintenance, handling & exchange process
- Waste disposal



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Tier 4 NOx: Areas of Concern

- No account for <u>carbon</u>, <u>ammonia slip</u>, fuel consumption and <u>practical/safety implications</u>
- <u>Catalyst deterioration</u> poorly known for zeolite, <u>real exhaust</u>, and <u>loco environment</u>
- References to truck "successes" are unprovening in durability and degradation
- Marine/Loco proposals are not consistent

Technical Basis:

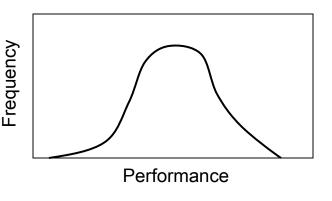
- Tier 2 engine-out NOx at 5.5g/hp-hr into SCR system
- Urea SCR only using a zeolite catalyst
- Locomotive exhaust temperature and duty cycle

Assessment Process

1. System Concept

2. Analytical Model

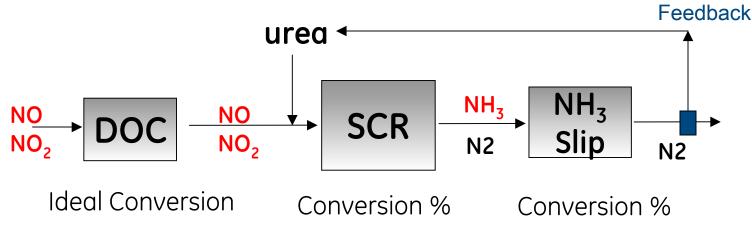
3. Monte Carlo Analysis





Urea-SCR: Nominal System Configuration

Three-Catalyst System:



- DOC design provides optimum NO/NO₂ ratio when new
- Slip catalyst converts NH_3 to N_2 , with some $NOx \& NH_3$
- 1.3g/bhp-hr requires 76% duty cycle NOx conversion at end of useful life
- Need ~85% peak conversion after degradation

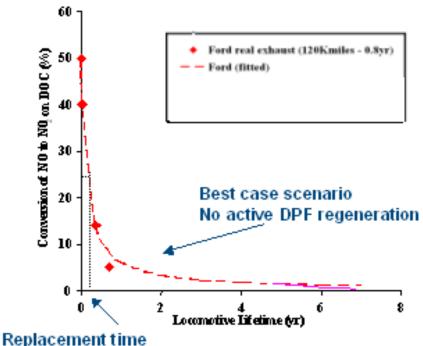


Nox

Sensor

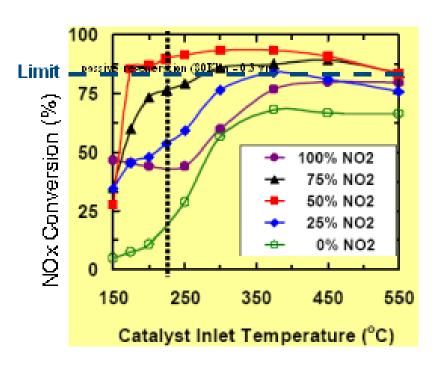
Deterioration - DOC

Deterioration under real exhaust



*Ref. C. Lambert, CLEERS, 2006, DEER 2006 SAE 2004-01-0072

Effect on SCR Performance:



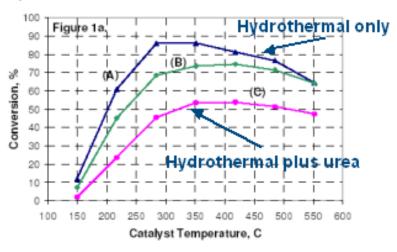
*Ref. J.H. Lee, General Motors, CLEERS, 2006

DOC will require replacement in <6 months



Deterioration - SCR

Hydrothermal vs. Chemical Deactivation

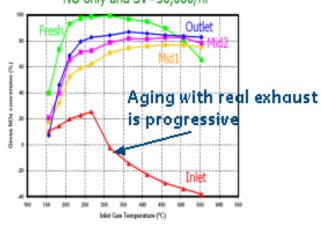


Ref. Ford & Pacific Northwest National Lab, North American Catalysis Society Meeting, Jun 2007, Session 4 Paper #50

"SCR catalysts that are engine aged with urea, deactivate in a more complicated manner than hydrothermal aging alone."

Ref. SAE 07PFL-397 in press 2007

Post Mortem of 120k mi SCR - Core#1 NO only and SV=30,000/hr



- · 120k mi engine aging of SCR catalyst upstream of filter was non-uniform
- Outlet of engine aged SCR correlates well to the 64hr/670°C hydrothermal aging
- Inlet was most severely aged work ongoing to understand

Ref. Ford. DEER 2006





Deterioration – Ammonia Slip Catalyst

Notch by notch dosing adjustment

Ref. BASF, SAE 2006-01-0640

- Deactivation of slip catalyst from 90%→ 80% ammonia conversion
- Assume selectivity to nitrogen remains at 80% (zero degradation)
- Inlet NOx for locomotive > trucks → higher ammonia slip levels
- Transient ammonia slip > 50 ppm possible due to large catalyst mass
- Potential to form N₂O due to NH₃ slip catalyst degradation
- Closed loop sensor needed technology not available today

At 1.3 g/hp-hr, ammonia slip will be above the odor threshold



Comparison of Loco and Trucks

- Exhaust temperature in a locomotive is higher than in a truck
- Trucks use V-based catalyst, not applicable to locomotives in US . . . Locomotives require Zeolite catalyst – not commercially available
- 120,000 miles on a truck is approximate 8 months of locomotive operation
- Ammonia slip concerns for locos
 - Continuous ammonia slip due to high dosing
 - Transient ammonia slip > 50 ppm possible due to large catalyst mass



SCR Limitations

- Rate Limited (temperature)
- Mass Transfer Limited (catalyst size)
- NH3 Limited (dosing accuracy & maldistribution)
- Thermal Aging / Poisoning (loss of sites)

Summary Assessment of Tier 4 NOx

- New catalyst entitlement consensus
- Larger impact of system interactions and variation
 - Deterioration of catalysts
 - ASC reconversion of NOx
 - Concern for ammonia slip
 - Full probabilistic analysis of variation
- High risk technology breakthroughs needed to get to <2.0 gm/HP-hr

Advances required
NOx Sensor accuracy
NOx Sensor variation
DOC catalyst replace
SCR degradation
SCR variation
ASC Selectivity
ASC conversion
Zeolite catalyst



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General Aftertreatment Constraints

Sensitive to Exhaust Temperature:

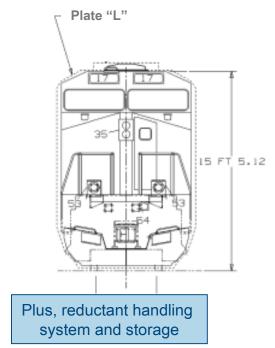
- Low temperature and low power/idle operation affects efficiency & soot loading
- High temperature, high altitude, tunnel operation affect durability

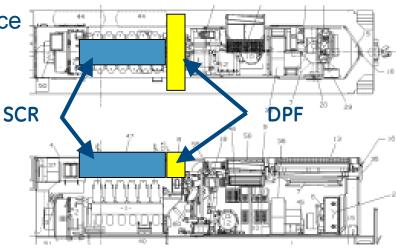
Packaging/Weight:

- Must mount above engine, limits device size and plumbing for reductant mixing
- High weight, will need significant structural support
- Impact to locomotive overall weight and balance

Mechanical Environment:

- Large housing, response to operating frequencies & thermal stress
- Shock loads due to hard couples, effect on substrate durability







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Fuel impact . . . new builds

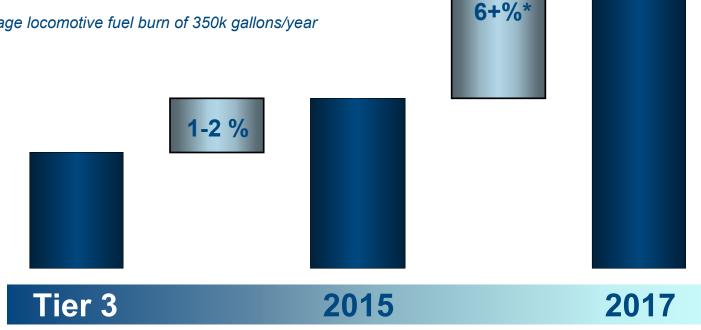
Each point of fuel efficiency loss drives:

An additional 3,500 gallons of fuel burned/year

An additional 35 tons of CO₂ exhausted/year

For every new locomotive

Assumes average locomotive fuel burn of 350k gallons/year



^{*} Includes fuel loss from the reduction in catalyst efficiency

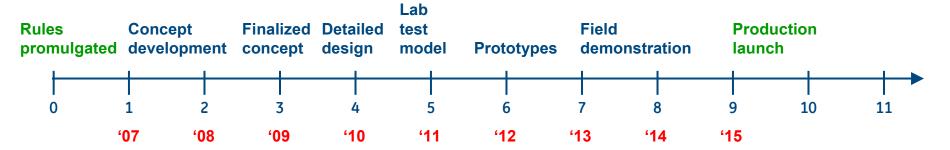


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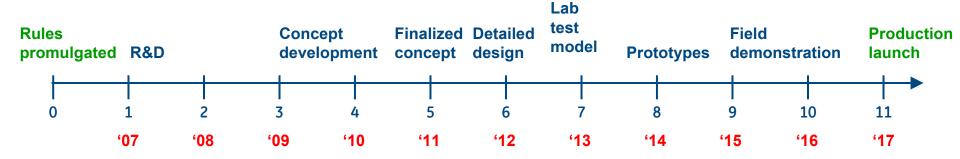


Tier 4 development timeline

Tier 4 PM



Tier 4 NOx



Based on successful Evolution launch . . . Already feeling schedule pressure



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